

METHOD FOR TEACHING WELDING TORCH ORIENTATION

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to a method for teaching a robot capable of implementing a proper torch orientation in performing welding work by play back operation of the robot supporting a torch for arc welding.

2. Description of the Related Art

Where a welding work is performed by play back operation of a robot supporting a welding torch (hereinafter referred to as torch), the orientation of the torch, as well as the position (three dimensional position) of its head, must be properly maintained during the movement of the robot. If the torch orientation is improper, a required welding work can not be accomplished even when the torch head moves on a welding path to trace properly a weld line. Especially, for a weld line path having a large curvature such as corner portion, teaching requiring the torch to sharply change its orientation should be avoided.

FIG. 1 schematically illustrates a conventional method of teaching the position and orientation of a torch to a robot, which is generally utilized. In FIG. 1, a path A→B→C→D→E→F is a welding path along a weld line, in which reference numeral 1 designates a torch mounted on a robot arm (not shown); and reference numeral 2 designates a tool center point set to the head of the torch 1. The tool center point 2 is set with a tool coordinate system of three rectangular X Y Z axes; the origin of the coordinate system is the tool center point 2, and one axis (Z axis) is coincident with the axial center of the torch 1. Thus, it is hereinafter defined that "torch position" refers to the position of the tool center point 2, that is, the origin of the coordinate system, and that "torch orientation" refers to the orientation of the coordinate system. Among many torches shown in FIG. 1, only the torch positioned at a start point A of the welding path is affixed by the reference numerals.

Now, with reference to FIG. 1, a conventional teaching procedure will be explained below.

(1) The robot is advanced by jog feed until the torch position (tool center point 2) coincides with the start point A of the welding path, and then the position of the start point A is taught to the robot. At this time, as torch orientation, an optimum welding orientation (the one shown as a) of the welding path starting from the start point A is taught.

(2) Without changing the taught orientation, the robot is moved along the welding path until the torch position coincides with a position PB located a little before a point B (path junction point B) at which the welding path is bent; and then the position PB is taught. As torch orientation, the orientation a having been taught at the point A is taught as it is.

(3) The robot is advanced further from the position PB until the torch position coincides with the path junction point B, and then the path junction point B is taught. As torch orientation, an intermediate orientation b' between an optimum orientation (given as b), as a welding orientation of the welding path starting from the start point B, and the orientation a having been taught at the start point A or the position PB is taught.

(4) The robot is advanced further from the point B until the torch position coincides with the position QB located a little beyond the path junction point B, and then the position QB is taught. As the torch orientation, the optimum orien-

tation b as the welding orientation of the welding path starting with the start point B is taught.

(5) Thereafter, the same operations are repeated to teach the positions of points PC, C, QC, PD, D, QD, PE, E, QE, and an end point F, and in addition, as the torch orientation, the orientations b, c', c, c, d', d, d, e', e, e at these points are taught.

The meanings of these codes are as follows:

c: Optimum torch orientation at path CD

d: Optimum torch orientation at path DE

e: Optimum torch orientation at path EF

c': Intermediate orientation between orientations c and d

d': Intermediate orientation between orientations d and e

However, in the above-mentioned conventional teaching method, and the end point F, the position and orientation of the points PB, QB, PC, QC . . . positioned near before and behind the junction points B, C . . . must be taught as well as the start point A, the junction points B, C . . . , so that there is a disadvantage that the teaching work load becomes large. Particularly, it requires a high skill and a long period of time to perform correctly teaching of the torch orientation affecting welding accuracy.

Particularly, the torch orientation at the point at which the welding path is bent, that is, the path junction points B, C . . . must be taught in such a manner that the change in the torch orientation must be smoothly performed in a small section ranging from before to behind these junction points. However, any simple and objective method for finding out such orientation is not available, thereby relying on the intuition and experience of an operator. Therefore, it is difficult to obtain a stable welding accuracy which is not influenced by the skillfulness of an operator.

OBJECTS AND SUMMARY OF THE INVENTION

An object of the present invention is to provide a method of teaching a robot capable of implementing a proper torch orientation in performing welding work by play back operation of the robot supporting a torch for arc welding, with a less work load.

The teaching according to the present invention follows substantially the following procedure:

(1) While advancing a robot by jog feed, the position of the start point and end point on a weld line defining a section, and of the junction points between these points are taught. However, instead of this teaching, there may be used either the position data of already prepared program or the position data prepared off line.

(2) A required torch welding orientation for respective sections is set on the basis of a reference plane.

(3) On the basis of both the position data of the junction points thus taught and the torch orientation set with respect to the sections starting from the junction points, a basic welding orientation for each section is calculated.

(4) One or a plurality of auxiliary points are set on the respective weld lines before and behind each junction point. Among these auxiliary points, for the most behind auxiliary point, the basic welding orientation for the section just before the present junction point is set, while for the most front auxiliary point, the basic welding orientation for the section starting from the present junction point is set. Further, the intermediate auxiliary points and junction points, with most behind and most front auxiliary points excluded, are given intermediate orientations between the basic welding orientations, which are

different from each other according to the arrangement order. The torch orientation is set so as to be changed smoothly near the junction points.

Using the method of the present invention, it is possible to produce automatically a program for realizing a desired torch orientation, by deliberately teaching only the position of the start point, the end point and junction points which divide the intermediate weld line into a plurality of sections, without paying a particular attention to the welding torch orientation. Further, in calculating the welding orientation, it is also possible to reflect the orientation around the torch axis which was taught at the beginning.

BRIEF DESCRIPTION OF THE DRAWINGS

The foregoing and other objects and feature of the invention will become apparent from the following description of preferred embodiments of the invention with respect to the accompanying drawings, in which:

FIG. 1 is a view for explaining a conventional method for teaching the position and orientation of a torch with respect to a robot, which is most generally used heretofore;

FIGS. 2A-2C are views showing sequentially a procedure for performing a method according to the present invention;

FIG. 3 is a view for explaining the orientation of a torch;

FIG. 4 is a view for explaining setting of a coordinate system and a reference plane for the sections AB, BC, and setting of a torch orientation based on the reference plane;

FIG. 5 is a view for explaining how to determine the coordinate system for the section AB;

FIG. 6 is a view illustrating an example of an operation screen for a torch orientation quick teach function;

FIG. 7 is a view illustrating an example of an automatic welding orientation calculating screen;

FIG. 8 is a view illustrating an execution screen for automatic calculation for smooth orientation change;

FIG. 9 illustrates, in the form of a major-part block diagram, the outline of the configuration of a welding robot system used in the present invention;

FIG. 10 is a view for explaining auxiliary points set before and behind the junction point B;

FIG. 11 is a view showing a circumference-shaped welding path connecting two semicircle sections; and

FIG. 12 is a flow chart describing the outline of an operation/processing procedure to be carried out after displaying of the operation screen of the torch orientation quick teach function.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

With reference to FIG. 9, the outline of the configuration of a robot system used in this embodiment will be explained. A central processing unit (hereinafter referred to as CPU) 11 in a robot controller 10 for controlling a welding robot is connected through a bus 20 with a memory 12 formed of a ROM, a memory 13 formed of a RAM, a nonvolatile memory 14, an axis controller 15, a teaching pendant 18 including a liquid crystal display (LCD) 17 and a general purpose interface 19.

The axis control part 15 is connected through a servo circuit 16 to a robot (body mechanism unit) 30. Also, the general purpose interface 19 is connected to a power source unit 40. The power source unit 40 has a function of controlling a welding voltage and welding current to be supplied to the torch 1 according to the instruction from the CPU 11.

The ROM 12 is stored with various programs by which the CPU 11 controls the robot (body mechanism unit) 30, the power source unit 40 and the robot controller 10 itself.

The RAM 13 is a memory utilized for the temporary storage and calculation of data. Also, the nonvolatile memory 14 is stored with various programs and parameter set values for specifying the content of the motion of the welding robot system. Programs and associated settings to cause the CPU 11 to execute various processing (whose contents will be described later) for embodying the present invention are divided into the ROM 12 and the nonvolatile memory 14 for storage.

A procedure for performing the teaching according to the present invention using the above-described welding robot system will be explained hereinafter.

Teaching method of the present invention is accomplished by performing the following three steps, that is, step (1), step (2) and step (3). The three steps correspond to FIGS. 2A, 2B, and 2C. The weld line A-F and the torch 1 in FIG. 2 are the same as those shown in FIG. 1.

1. [Step (1)]

At this step, the position data of respective points including the start point A, end point F, and intermediate path junction points B, C, . . . E on the welding path is obtained.

This work is accomplished, as shown in FIG. 2A, by advancing the robot by jog feed to cause the respective torch positions (tool center point 2) to be coincident with the start point A, end point F, and intermediate path junction points B, C, . . . E on the welding path, and then teaching the position of the respective points to the robot. At that time, although the torch orientation is to be also simultaneously taught, the torch orientation is not considered at this step.

At this step, instead the above-mentioned teaching, either the position data of already prepared program relating to the respective points A through F or the position data (orientation data is not necessary) prepared off line may be transferred to the robot controller 10.

2. [Step (2)]

At this step, the welding orientation (hereinafter referred to as basic orientation) which is believed to be optimum for each of the sections AB, BC, . . . EF is automatically calculated.

First, a reference plane for defining the torch orientation is specified, and then an angle parameter representing the orientation is inputted into the robot controller 10. Then, on the basis of the inputted angle parameter and the position data taught at the above-mentioned step(1), the welding orientation (basic orientation) which is believed to be optimum for each of the sections is determined by the software processing of automatic calculation, and the calculated results is stored in the nonvolatile memory 14. This causes the program including the position data obtained by the teaching at step (1) to be transformed into a program teaching the torch orientation as shown in FIG. 2B.

In FIG. 2B, the orientation a calculated for the start point A is a torch orientation which is believed to be optimum for the welding in the section AB; the orientation b calculated for the start point B is a torch orientation which is believed to be optimum for the welding in the section BC; and hereafter in the same manner, the orientation e calculated for the start point E is a torch orientation which is believed to be optimum for the welding in the section EF. These orientations a, b . . . e represent basic orientations in the respective sections. The basic orientation e at the end point F is the same as the basic orientation e in the section E-F including the end point F.

The parameters to be inputted to calculate the basic orientation and a method for calculating the basic orientation

will be explained hereinafter. First, with reference to FIG. 3, the reference plane and the angle parameters (inclination angle and forward angle) will be explained.

First, a reference plane, which is used as a reference for specifying an inclination angle described later, is set. FIG. 3 shows a relationship among the reference plane, the inclination angle and the forward angle, taking the path A-B as an example. A reference plane β , though set by teaching the reference plane to the robot as described later, can be replaced by a known plane such as a robot installing plane. The reference plane may be also set by inputting directly the data specifying the normal vector of the reference plane.

When assuming a plane γ on which a straight line representing the direction of the torch 1 (Z-axis direction of a tool coordinate system) is placed with respect to the reference plane β , an angle between the plane γ and the reference plane β is defined as an "inclination angle θ ". When standing a vertical line g to the straight line A-B representing the welding path from the tool center point 2 in a manner such that it is placed on the plane γ , an angle between the straight line representing the direction of the torch 1 (Z-axis direction of a tool coordinate system) and the straight line g is defined as a "forward-angle ϕ ";

When the reference plane β was set, then a three dimensional rectangular coordinate system for calculating the torch orientation is set for each path by using the vector in the path direction and the normal vector of the reference plane. The torch orientation is expressed by a 3x3 matrix corresponding to the orientation expressing part of a 4x4 homogeneous transformation matrix representing the position/orientation of the tool coordinate system. The matrix is composed of three rectangular unit vectors, that is, a normal vector $\langle N \rangle$, an orientation vector $\langle O \rangle$ and an approach vector $\langle A \rangle$. Thus, the vector $\langle N \rangle \langle O \rangle \langle A \rangle$ representing the tool orientation is called a tool vector.

Hereafter, it is defined that " $\langle \rangle$ " represents a vector; " \times " and " \cdot " placed between vectors indicate an outer product and an inner product respectively.

FIG. 4 is a view showing how to define the coordinate system, the reference plane β , the inclination angle θ and the forward angle ϕ , taking the sections AB, BC as an example. In this manner, one coordinate system is made for corresponding one section (such as AB or BC). Therefore it is possible to specify a torch orientation (tool vector) with respect to the corresponding weld line by calculating the torch orientation in a manner such that the inclination angle θ and the forward angle ϕ specified on the coordinate system are satisfied. With reference to FIG. 5 and other figures, the embodiment of the present invention will be specifically explained hereinafter.

2. a: How to define a coordinate system for the section AB (refer to FIG. 5)

A unit vector $\langle U \rangle$ in the direction from the point A to the point B is calculated by the following equation [1], and the vector is taken as the X-axis of a coordinate system to be determined.

$$\langle U \rangle = \langle AB \rangle / |\langle AB \rangle| \quad [1]$$

where " $|\langle \rangle|$ " represents the absolute value of the vector.

Then, the outer product $\langle V \rangle$ of a normal vector $\langle n \rangle$ of the reference plane and the unit vector $\langle U \rangle$ in the X-axis direction is calculated by the following equation [2], and the product is taken as the Y-axis of a coordinate system to be determined.

$$\langle V \rangle = \langle n \rangle \times \langle U \rangle / |\langle n \rangle \times \langle U \rangle| \quad [2]$$

Finally, the outer product $\langle W \rangle$ of $\langle U \rangle$ and $\langle V \rangle$ is calculated, and the product is taken as the Z-axis of a

coordinate system. As described above, from the direction of the section (A-B) and the normal vector $\langle n \rangle$ of the reference plane, the XYZ coordinate in this section can be set. Therefore, in setting a coordinate system in a section, it does not matter whether the direction of the section is within the reference plane. For example, even when the line connecting the point A and point B is not placed on the reference plane β , the X-axis is set in the direction A-B; the Y-axis, in the direction perpendicular to the X-axis and the normal line of the reference plane; and the Z-axis, in the direction perpendicular to the X-axis and the Y-axis.

Hereafter, in this manner, for each of the sections AB, BC . . . , respective coordinate system (which system is hereinafter called [UVW]) is defined, and for each section on the coordinate system [UVW], the inclination angle θ and the ϕ is specified.

2. b: How to calculate the torch orientation (tool vector) implementing the specified inclination angle θ and the forward angle ϕ on the determined coordinate system [UVW]

The matter to be paid attention when calculating the torch orientation is that, in a general robot having six degrees of freedom, the torch orientation can be unconditionally defined only by determining a spin angle (an angle representing the orientation of a rotation around the axis of the torch 1 or around the Z-axis of the tool coordinate system) in addition to the inclination angle θ and the forward angle ϕ .

In this embodiment, in determining the spin angle, a method is employed in which the spin angle at the above-mentioned step (1) is caused to be reflected in the torch orientation which has been transformed to the program data corresponding to FIG. 2B from the program data corresponding to FIG. 2A. This method has an advantage in that a-twining-of welding cable at the time of playing back operation or an interference with a work piece due to the rotation of the robot wrist around the torch is made hard to occur. The processing including the determination of the spin angle will be explained hereinafter.

2. b.1: From the orientation data at the teaching of the point A, the taught spin angle (taught_spin_ang) is determined. During determining process of the taught spin angle, although the inclination angle and the forward angle at the time of teaching are also calculated, the data thereof becomes unnecessary.

2. b.1.1: Using the equation [3], the tool vector $\langle N \rangle \langle O \rangle \langle A \rangle$ representing the tool orientation at the time of teaching is transformed to the expression ${}^P\langle N \rangle {}^P\langle O \rangle {}^P\langle A \rangle$ on the coordinate system [UVW] having been already determined for each section. In the expression, the upper left subscript P is used as a code for meaning the expression on the coordinate system [UVW].

$$[{}^P\langle N \rangle, {}^P\langle O \rangle, {}^P\langle A \rangle] = [\langle U \rangle \langle V \rangle \langle W \rangle]^{-1} \cdot [\langle U \rangle \langle V \rangle \langle W \rangle] \quad [3]$$

where $[\]^{-1}$ represents the inverse matrix of the matrix $[\]$.

2. b.1.2: The taught inclination angle at the time of teaching (expressed as taught_incl_ang) is calculated by the following equation [4].

$$\text{taught_incl_ang} = \text{atan2}({}^PA_z, {}^PA_y) \quad [4]$$

In the equation, ${}^PA_z, {}^PA_y$ are components in the Z-axis and Y-axis of ${}^P\langle A \rangle$; and $\text{atan2}(\xi_1, \xi_2)$ is in general a function which gives an output of angle ψ from inputs of ξ_1 and ξ_2 , in which $\cos(\psi) = \xi_1$ and $\sin(\psi) = \xi_2$ holds.

2. b.1.3: Calculation of forward angle at the time of teaching (taught_fwrd_ang)

First, the tool vector [$P<N>$ $P<O>$ $P<A>$] at the time of teaching is turned around $<U>$ as the X-axis of the coordinate system [UVW] by $(\pi/2 - \text{taught_fwr_ang})$ to produce a tool vector [$P<N'>$ $P<O'>$ $P<A'>$] representing a condition in which an approach vector (an unit vector representing the torch direction) is placed on the X-Z plane of the coordinate system [UVW]. This is determined by the following equation [6], using the next equation [5].

$$\theta_1 = (\pi/2 - \text{taught_fwr_ang}) \quad [5]$$

$$[P<N'> P<O'> P<A'>] = \begin{pmatrix} 1 & 0 & 0 \\ 0 & C\theta_1 & -S\theta_1 \\ 0 & S\theta_1 & C\theta_1 \end{pmatrix} * [P<N> P<O> P<A>] \quad [6]$$

In the equation [6], $C\theta_1$ and $-S\theta_1$ represent $\sin \theta_1$ and $\cos \theta_1$, respectively (hereafter, in the same manner).

The forward angle at the time of teaching (taught_fwr_ang) is given by the following equation [7].

$$\text{taught_incl_ang} = \text{atan2}(P A'x, P A'z) \quad [7]$$

where $P A'x, P A'z$ are components in the X-axis and Z-axis of $P<A'>$.

2. b.1.4: Calculation of spin angle at the time of teaching (taught_spin_ang)

First, the previously determined tool vector [$P<N'>$ $P<O'>$ $P<A'>$] is rotated as the Y-axis of the coordinate system [UVW] by an angle of taught_fwr_ang around $<V>$ to produce a tool vector [$P<N''>$ $P<O''>$ $P<A''>$] representing a condition in which an approach vector (an unit vector representing the torch direction) is coincident with $<W>$ which is the Z-axis of the coordinate system [UVW]. This is determined by the following equation [9], using the next equation [8].

$$\theta_2 = \text{taught_fwr_ang} \quad [8]$$

$$[P<N''> P<O''> P<A''>] = \begin{pmatrix} C\theta_2 & 0 & S\theta_2 \\ 0 & 1 & 0 \\ -S\theta_2 & 0 & C\theta_2 \end{pmatrix} * [P<N'> P<O'> P<A'>] \quad [9]$$

Then, the spin angle at the time of teaching (taught_spin_ang) is determined by the following equation [10].

$$\text{taught_spin_ang} = \text{atan2}(P N''y, P N''x) \quad [10]$$

2. b.2: From the calculated spin angle at the time of teaching expressed as (taught_spin_ang), and the inclination angle specified by inputting (expressed as incl_ang) and the forward angle (expressed as fwr_ang), a tool vector representing the target torch orientation is calculated.

2. b.2.1: A transformation matrix is determined which represents the rotation with the same magnitude as taught_spin_ang around $<W>$ which is the Z-axis of the coordinate system [UVW]. That is, the matrix applying the rotation to the unit matrix is determined. This is determined by the following equation [12], using the next equation [11].

$$\theta_3 = \text{taught_spin_ang} \quad [11]$$

$$[P<N> P<O> P<A>] = \begin{pmatrix} C\theta_3 & -S\theta_3 & 0 \\ S\theta_3 & C\theta_3 & 0 \\ 0 & 0 & 1 \end{pmatrix} \quad [12]$$

2. b.2.2: [$P<N>$ $P<O>$ $P<A>$] is rotated around the Y-axis ($<V>$) of the coordinate system [UVW] by $-\text{fwr_ang}$. This is determined by the following equation [14], using the next equation [13].

$$\theta_4 = -\text{fwr_ang} \quad [13]$$

$$[P<N'> P<O'> P<A'>] = \begin{pmatrix} C\theta_4 & 0 & S\theta_4 \\ 0 & 1 & 0 \\ -S\theta_4 & 0 & C\theta_4 \end{pmatrix} * [P<N'> P<O'> P<A'>] \quad [14]$$

2. b.2.3: [$P<N'>$ $P<O'>$ $P<A'>$] is rotated around the X-axis ($<U>$) of the coordinate system [UVW] by $\text{incl_ang} - \pi/2$. This is determined by the following equation [16] using the next equation [15].

$$\theta_5 = -\text{incl_ang} - \pi/2 \quad [15]$$

$$[P<N'> P<O'> P<A'>] = \begin{pmatrix} 1 & 0 & 0 \\ 0 & C\theta_5 & 0 \\ 0 & S\theta_5 & C\theta_5 \end{pmatrix} * [P<N'> P<O'> P<A'>] \quad [16]$$

2. b.2.4: The calculated tool vector [$P<N'>$ $P<O'>$ $P<A'>$] is transformed to the expression [$<n'>$ $<o'>$ $<a'>$] on the base coordinate system [UVW] which has been set to the robot. This is given by the following equation [17].

$$[<n'> <o'> <a'>] = [<U> <V> <W>] * [P<N'> P<O'> P<A'>] \quad [17]$$

By calculating the above calculation on the respective sections AB, BC . . . EF, a tool vector can be calculated which represents the basic welding orientation (refer to FIG. 2B) at the respective points A, B . . . E.

3. [Step (3)]

At this step, an automatic calculation is executed by software processings, which, using the program where the basic welding orientations shown in FIG. 2B are taught, produces a program which realizes a smooth transition of the torch orientation in the subsection ranging from behind to before respective junction points by adding auxiliary points near the junction points B, C . . . E. The calculated results are stored in the nonvolatile memory 14. This provides a program which is expected to have the same quality as is taught carefully by a skilled operator in the conventional method (refer to FIG. 1).

In this embodiment, auxiliary points are added before and behind respective junction points. However, the points may be added to only front or only behind the junction points. When the position of the auxiliary points has been determined by the automatic calculation, tool vectors at the added respective auxiliary points and at the respective junction points are calculated to realize a smooth transition of the torch orientation near the junction points.

Generally, the taught orientation at the junction points B, C . . . E becomes different from the basic welding orientation at the junction points B, C . . . E shown in FIG. 2B. That is, the taught orientation is brought close to the basic welding orientation at the junction point immediately behind the present junction point. For example, the taught orientation at the junction point B is brought close to the basic welding orientation at the start point A; and the taught orientation at the junction point C is brought close to the basic welding orientation at the start point B.

The method of calculating the position of the auxiliary points to be added, and the method of calculating respective junction points and tool vectors at the respective junction points will be sequentially explained hereinafter. For the start point A and the end point F, the basic welding orientations determined for the path AB and EF are used respectively as the taught orientation.

Although the number of added auxiliary points to be added may be two or more in all, including auxiliary points before and behind the junction point, according to the

specification of the user, here the number is determined four including two points before and two points behind the junction point. FIG. 10 is a view for explaining how to determine the position of auxiliary points when two auxiliary points each are provided before and behind the junction point B connecting the straight-line section AB with the straight-line section BC.

A tool vector representing the orientation at the respective points a, b, c, d, e of FIG. 10 is calculated. Of those points, the points a, b, d, e are auxiliary points, while the point c is a point coincident with the junction point B. It is assumed that the distances between adjacent points are equal to each other, that is, $ab=bc=cd=de$ (=pitch). At the points a through e, there is determined by calculation an intermediate orientation between the orientation (here a basic welding orientation determined for the point A) for the front side path A-B with respect to the junction point B and the orientation (here a basic welding orientation determined for the point B) for the rear side path B-C.

Here, it is assumed that the orientation at the auxiliary point a is made to be coincide with the basic welding orientation determined for the start point A, while the orientation at the auxiliary point e is made to be coincide with the basic welding orientation determined for the junction point B. Tool vectors at the midway auxiliary points b, c, d is determined in equally dividing relationship so that the torch orientation is smoothly changed through four small sections ab, bc, cd, de. The calculation of the position of auxiliary points and the method of specifically calculating the equal division of orientation will be explained herein-after.

3. a: Calculation of position of auxiliary points a, b to be set on path A-B in front of junction point B

The auxiliary points a, b should be defined by the following equations [18] through [20]. The meaning of codes used here is taken as follows:

n: Number of auxiliary points to be set in front of (or behind) junction point B (user set value, two in case of FIG. 10) pitch: Auxiliary point inserting interval (user set value)

<P1>: Vector representing point A

<P2>: Vector representing point B

i: Auxiliary point number ($i=0$ for a, $i=1$ for b, in case of FIG. 10)

: Vector going from point B toward the i-th auxiliary point

<Pai>: Vector representing the i-th auxiliary point determined by calculation

$$\langle Li \rangle = \frac{\langle p1 \rangle - \langle p2 \rangle}{|\langle p1 \rangle - \langle p2 \rangle|} * \text{pitch} * (n - i) \quad [18]$$

$$\langle Pai \rangle = \langle p2 \rangle + \langle Li \rangle \quad [19]$$

$$= \langle p2 \rangle + \frac{\langle p1 \rangle - \langle p2 \rangle}{|\langle p1 \rangle - \langle p2 \rangle|} * \text{pitch} * (n - i) \quad [20]$$

3. b: Calculation of position of auxiliary points d, e set on path B-C on the rear side of junction point B

This calculation is made by the calculation similar to the above-described 3. a. Therefore, the description of the calculation equations will be omitted.

3. c: Calculation of orientation at auxiliary points

With a change in the orientation at a junction point taken as a change from an orientation 1 to an orientation 2, a method of calculating an intermediate orientation between the orientation 1 and the orientation 2 will be explained. Hereafter, codes i and n are taken as the following meanings;

n: Number of auxiliary points on path in front of junction point B (=number of auxiliary points on path on rear side of junction point) (both are user set values)

i: Auxiliary point number ($0 \leq i \leq 2n$; in case of $n=2$, $i=0, 1, 2, 3, 4$)

weld_dir_vec 1: Unit vector representing advance direction of the path in front of junction point

weld_dir_vec 2: Unit vector representing advance direction of the path on rear side of junction point

[<Ns> <Os> <As>]: Tool vector corresponding to orientation 1

[<Ne> <Oe> <Ae>]: Tool vector corresponding to orientation 2

<k0>: Normal vector of plane including weld_dir_vec 1 and weld_dir_vec 2 (generally not unit vector)

t0: Angle between weld_dir_vec 1 and weld_dir_vec 2
3. c. 1: Calculation of vector <k0> and angle t0 (calculation of orientation 2')

The vector <k0> is calculated by the following equation:

$$\langle k0 \rangle = \text{weld_dir_vec } 1 \times \text{weld_dir_vec } 2 \quad [21]$$

s0, a sine of an angle between a vector weld_dir_vec 1 and a vector weld_dir_vec 2, and c0, a cosine of the angle are given by the following equations [22] and [23], respectively:

$$s0 = |\langle k0 \rangle| \quad [22]$$

$$c0 = \text{weld_dir_vec } 1 \cdot \text{weld_dir_vec } 2 \quad [23]$$

Also, the angle t0 is given by the following equation [24]:

$$t0 = \text{atan2}(s0, c0) \quad [24]$$

Then, a vector [<Ne'> <Oe'> <Ae'>] corresponding to the orientation 2' which is obtained by rotating the orientation 2 around the vector <k0> by an angle -t0 is calculated by the following equation [25]:

$$[\langle Ne' \rangle \langle Oe' \rangle \langle Ae' \rangle] = \text{Rot}(\langle k0 \rangle, -t0) * [\langle Ne \rangle \langle Oe \rangle \langle Ae \rangle] \quad [25]$$

Generally, Rot(<V>, θ) represents a transformation matrix performing the rotation of an angle θ around the vector <V>.

However, if s0 is a very small positive number, then the following settings may be possible:

$$\langle k0 \rangle = (1.0 \ 0.0 \ 0.0) \quad [26]$$

$$t0 = 0.0 \quad [27]$$

$$[\langle Ne' \rangle \langle Oe' \rangle \langle Ae' \rangle] = [\langle Ne \rangle \langle Oe \rangle \langle Ae \rangle] \quad [28]$$

Where the vector <V> is a unit vector, and when the following equations are set:

$$\langle V \rangle = \begin{bmatrix} vx \\ vy \\ vz \end{bmatrix},$$

$$\text{vers}\theta = 1 - \cos\theta,$$

Rot(<V>, θ) is given by the following equation [29]. If <V> is not a unit vector, a unit vector is obtained by dividing respective elements of <V> by |<V>| before calculating the equation [29].

$$R(\langle V \rangle, \theta) = \begin{pmatrix} vx*vx*vers\theta + \cos \theta & vy*vx*vers\theta + vz*\sin \theta & vz*vx*vers\theta + vx*\sin \theta \\ vx*vy*vers\theta + vz*\sin \theta & vy*vy*vers\theta + \cos \theta & vz*vy*vers\theta + vx*\sin \theta \\ vx*vz*vers\theta + vz*\sin \theta & vy*vz*vers\theta + vx*\sin \theta & vz*vz*vers\theta + \cos \theta \end{pmatrix} \quad [29]$$

3. c. 2: Calculation of $\langle k1 \rangle$ and $t1$ (calculation of orientation 1')

The orientation 2' determined in the above paragraph, 3. c. 1 corresponds to the one which is obtained by rotating the orientation 2 (so as to be brought close to the orientation 1) around the normal of a plane including the welding path before and behind a junction point. Now, as a process for further eliminating a difference between the orientation 2' and the orientation 1, a transformation will be considered in which both approach vectors are superposed on each other.

First, the approach vector of the orientation 1 is superposed on the approach vector of the orientation 2' by a shortest rotation to produce the orientation 1'. The vector acting as a rotating center at that time is taken as $\langle k1 \rangle$; and the rotational angle, as $t1$ ($0 \leq t1 \leq \pi$). The description of equations [30] through [34] representing $\langle k1 \rangle$, $t1$ and the related quantity is as follows:

$$\langle k1 \rangle = \langle As \rangle \times \langle Ae \rangle \quad [30]$$

$$s1 = |\langle k1 \rangle| \quad [31]$$

where if $s1$ is a very small positive number, the following setting [32] will be also possible:

$$k1 = \langle Ne \rangle \quad [32]$$

$$c1 = \langle As \rangle \cdot \langle Ae \rangle \quad [33]$$

$$t1 = \text{atan2}(s1, c1) \quad [34]$$

where, note that atan2 is outputted (defined) even when $s1=0$ is inputted.

Then, the orientation 1' obtained by rotating the orientation 1 around the vector $\langle k1 \rangle$ by the angle $t1$ is calculated. A tool vector $[\langle Ns \rangle \langle Os \rangle \langle As \rangle]$ corresponding to the orientation 1' is given by the following [35]:

$$[\langle Ns \rangle \langle Os \rangle \langle As \rangle] = \text{Rot}(\langle k1 \rangle, t1) * [\langle Ns \rangle \langle Os \rangle \langle As \rangle] \quad [35]$$

3. c. 3: Calculation of $\langle k2 \rangle$ and $t2$

With respect to the direction around an approach vector, there is a deviation between the orientation 2' calculated in the above paragraphs, 3. c. 1 and 3. c. 2, and the orientation 1'. Thus, as a process for eliminating the deviation between the both, a rotational transformation for removing the deviation will be considered.

A vector acting as a rotational center is taken as $\langle k2 \rangle$; and the rotational angle, as $t2$ ($0 \leq t2 \leq \pi$). $\langle k2 \rangle$ is an approach vector of both orientations or a vector obtained by making the approach vector reversal. The description of equations [36] through [40] representing $\langle k2 \rangle$, $t2$ and the related quantity are as follows:

$$\langle k2 \rangle = \langle Ns \rangle \times \langle Ne \rangle \quad [36]$$

$$s2 = |\langle k2 \rangle| \quad [37]$$

where if $s2$ is a very small positive number, the following setting [38] may be possible:

$$k2 = \langle Ae \rangle \quad [38]$$

$$c2 = \langle Ns \rangle \cdot \langle Ne \rangle \quad [39]$$

$$t2 = \text{atan2}(s2, c2) \quad [40]$$

Note that atan2 is outputted (defined) even when $s2=0$ is inputted.

Now, the vectors $\langle k2 \rangle$ and $\langle Ae \rangle$ are vectors facing each other in the same or reverse direction, and whether the direction is same or reverse can be judged by the sign of the inner product of both if calculated. Thus, "save_sign" is defined as follows:

$$\text{save_sign} = \langle k2 \rangle \cdot \langle Ae \rangle \quad [41]$$

The sign of save_sign is utilized later for judging of processing.

3. c. 4: Equal division processing

Considering the total number of auxiliary points before and behind junction points and the junction points themselves, the number h of orientations to be calculated for one junction point is given as $h=2n+1$ (in the example of FIG. 10, $n=2$, thus $h=5$, so that total number is five for points a through e).

First, a vector $[\langle N1 \rangle \langle O1 \rangle \langle A1 \rangle]$ corresponding to an orientation obtained by rotating the orientation 1 around the vector $\langle k0 \rangle$ by $t0 * i/2n$ is determined by the following equation [42].

$$[\langle N1 \rangle \langle O1 \rangle \langle A1 \rangle] = \text{Rot}(\langle k0 \rangle, (t0 * i/2n)) * [\langle Ns \rangle \langle Os \rangle \langle As \rangle] \quad [42]$$

Further, an orientation $\langle k1 \rangle$ obtained by rotating the vector $\langle k1 \rangle$ around the vector $\langle k0 \rangle$ by $t0 * i/2n$ is determined by the following equation [43].

$$\langle k1 \rangle = \text{Rot}(\langle k0 \rangle, (t0 * i/2n)) * \langle k1 \rangle \quad [43]$$

Then, $[\langle N2 \rangle \langle O2 \rangle \langle A2 \rangle]$ obtained by rotating $[\langle N1 \rangle \langle O1 \rangle \langle A1 \rangle]$ around $\langle k1 \rangle$ by $t1 * i/2n$ is determined by the following equation [44].

$$[\langle N2 \rangle \langle O2 \rangle \langle A2 \rangle] = \text{Rot}(\langle k1 \rangle, (t1 * i/2n)) * [\langle N1 \rangle \langle O1 \rangle \langle A1 \rangle] \quad [44]$$

Further, according to the sign of save_sign , $\langle k2 \rangle$ is defined as follows:

$$\text{For save_sign} < 0: \langle k2 \rangle = -A2 \quad [45]$$

$$\text{For save_sign} \geq 0: \langle k2 \rangle = A2 \quad [46]$$

Finally, $[\langle Ni \rangle \langle Oi \rangle \langle Ai \rangle]$ obtained by rotating $[\langle N2 \rangle \langle O2 \rangle \langle A2 \rangle]$ around $\langle k2 \rangle$ by $t2 * i/2n$ is determined by the following equation [47].

$$[\langle Ni \rangle \langle Oi \rangle \langle Ai \rangle] = \text{Rot}(\langle k2 \rangle, (t2 * i/2n)) * [\langle N2 \rangle \langle O2 \rangle \langle A2 \rangle] \quad [47]$$

By performing the processing including the above-described calculation contents on individual junction points, the position of auxiliary points in the above paragraphs, 3. a and 3. b, and the orientation at the auxiliary points (and junction points) in the paragraph, 3. c are determined. Therefore, by combining them, all position data relating to respective junction points will be obtained.

4. [Teaching processing]

On the basis of the above-mentioned description, the procedure and processing of the teaching method in this embodiment, mainly the operation an operator performs, will be further explained hereinafter.

[Preparation]

(1) First, for the preparation to perform the teaching of the torch orientation, the operator teaches sequentially the start point, end point and junction points on the welding path as shown in FIG. 2A by jog feed without paying any attention to the torch orientation as the data for motion program. It is preferable, during the teaching, to avoid a change of torch orientation which will induce a cable twining.

(2) Then, an operation screen of the torch orientation quick teach function is displayed on the LCD 17 of the teaching pendant 18. This is shown in FIG. 6.

[Operation/processing execution procedure]

With reference to the flow chart of FIG. 12, the outline of the operation/processing execution procedure after the operation screen of the torch orientation quick teach function is displayed will be explained.

(3) First, a program name ("TEST") of a program which becomes a transformation source and is taught in the [preparation 1] is inputted (step S1), and then a scope to be transformed is specified (steps S2 through S5). The transformation scope is specified in such a manner that either whole or part of the program be selected (step S2), and in case of part (step S3), the selected scope be specified with the row numbers (numbers of a transformation start row and transformation end row) of the program (steps S4, S5).

(4) Then, whether the transformed part is newly "produced", or "replaced" by part specified by the transformation source is set (step S6). When nothing is set at the step, "replaced" is considered to be set.

(5) When "produced" is set at the above-mentioned (4) (step S7), the program name of the program destined to be transformed is inputted (step S8), however when "replaced" is set, the operation to input the program name of the program destined to be transformed is not required.

(6) If the program name inputted in the above-mentioned (5) has been registered, the number of the row corresponding to the transformed part to be inserted is set. Where the program is an unregistered (newly produced) program, such setting is not required.

(7) Then, the page switching key is depressed to cause "Welding orientation automatic calculation screen" to be displayed on the screen of the LCD 17. This is shown in FIG. 7.

(8) On "Welding orientation automatic calculation screen", first, whether the reference plane which is a plane used for setting an inclination angle is taught or not is set by selecting "Yes" or "No". When the reference plane is not set by teaching, the plane parallel to the robot installing plane (floor plane) is considered to be set as the reference plane. The data on the reference plane is given in the form of the data on normal vectors. The direction of the reference plane is specified by the direction of the normal vector.

(9) When in the above-mentioned (8), the teaching of the reference plane is selected (step S9), the reference plane is taught (step 10). Using a teaching pendant 18, the torch head is caused to move by the jog feed operation, and the position of three points (provided that the points be selected in a condition in which they are not located on one straight line) on the reference plane desired to be set should be taught. The torch orientation at the time of teaching is optional.

(10) The inclination angle θ and the forward angle ϕ desired for each section should be inputted with a numerical value (steps S11, S12).

(11) To execute the processing of "Torch orientation automatic calculation", the function key "TRANSFORMATION" should be depressed. This causes the processing of "Torch orientation automatic calculation" to be started,

whereby the basic welding orientation satisfying the conditions of the desired inclination angle θ and the forward angle ϕ is calculated for each section (refer to FIG. 2B).

Now, let corner part be a part where in which a straight-line section with a length more than a predetermined value crosses at a junction point with another straight-line section with a length more than a predetermined value, for example, a part in which on the weld line of FIG. 2B, the straight-line section B-C crosses at the connection point C with the straight-line section C-D. If the weld line has no corner part (step S13), this means that there is no junction point for which "Calculation for smooth orientation change" must be executed, or the welded line, so that the welding program will be completed at this step.

For example, this applies to a case where two semicircle paths (HIJ and JKH) are connected into a circle to weld the circumference, as shown in FIG. 11. In such a case, the X-axis direction of the coordinate system [UVW] set on each of points H through K is specified at the tangent line direction at each of the points H through K on the circular arc path, so that the basic welding orientation at the points H through K is calculated by the above-mentioned calculation process.

(12) On the contrary, when the weld line has a corner part, the page switching key should be further depressed to cause the execution screen of "Automatic calculation for smooth orientation change" to be displayed. This is shown in FIG. 8.

(13) In this screen, first, the number n of auxiliary points to be inserted into positions before and behind a junction point forming the corner part is set (step S14). FIG. 10 shows an example in which $n=2$ is set.

(14) Then, the inserting interval (the above-mentioned "pitch") of auxiliary points should be inputted with a numerical value (step 15).

(15) Finally, depressing the function key "EXECUTION" of the teaching pendant 18 causes the processing of the automatic calculation for smooth orientation change to be executed (step 16). Here, for junction points forming the corner part in the path programmed within the scope specified by the program (TEST), the position of auxiliary points is calculated under the above-mentioned set condition (n , pitch), and then, a welding program for realizing a smooth torch orientation change (transition) is automatically produced (step S17).